

NO reduction and CO oxidation over Cu/Ce/Mg/Al mixed oxide catalyst in FCC operation

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Abstract

Simultaneous NO reduction and CO oxidation in the presence of O₂, H₂O and SO₂ over Cu/Mg/Al/O (Cu-cat), Ce/Mg/Al/O (Ce-cat) and Cu/Ce/Mg/Al/O (CuCe-cat) were studied. At low temperatures (<340 °C), the presence of O₂ or H₂O enhanced the activity of CuCe-cat for NO and CO conversions, but significantly suppressed the activity of Cu-cat and Ce-cat. At high temperature (720 °C), the presence of O₂ or H₂O had no adverse effect on the NO and CO conversions over these catalysts. The addition of SO₂ to NO + CO + O₂ + H₂O system had no effect on the reaction of CO + O₂ over Cu-cat, but deactivated this catalyst for NO + CO and CO + H₂O reactions; over Ce-cat, all of these reactions of NO + CO, CO + O₂ and CO + H₂O were suppressed significantly; over CuCe-cat, NO + CO and CO + O₂ reactions were not affected while the reaction of CO + H₂O was slightly inhibited. © 2002 Elsevier Science B.V. All rights reserved.

Keywords: NO reduction; CO oxidation; FCC; H₂O and SO₂ poisoning; NO and CO co-adsorption

1. Introduction

The reduction of NO by CO is the most ideal way to remove simultaneously NO and CO from industrial effluents, and therefore, it has received particular attention [1–3]. Copper-based catalysts show a high activity in the conversion of nitrogen oxides (NO_x) to N₂ [2–4]. However, the deactivation caused by copper oxide aggregation or SO₂ poisoning is still an unsolved problem [5]. Cerium oxide has been widely used in the automotive three-way catalytic converter

as an oxygen storage medium and thermal stabilizer. The addition of ceria to precious metal (Pd, Pt, Rh) can strongly improve the catalyst performance [6,7]. Several binary mixtures of transition metal and ceria have been proposed in literature [8–10].

In the regenerator of fluid catalytic cracking units (FCC, the principal gasoline-producing process in the refinery; for details see Ref. [11]), the high-temperature flue gas (650–760 °C) contains NO, NO₂, O₂, CO, CO₂, SO₂, SO₃, H₂O simultaneously. Therefore, the FCC regenerator poses a very challenging problem for controlling NO_x [12]. In the dense phase bed of the FCC regenerator, the CO concentration is much higher than the O₂ concentration [11]. A CO combustion promoter is usually used in industrial operations to control the emission of CO. However, the use of this promoter increases the

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NO_x emissions [13]. In this paper, we report a cerium-promoted Cu/Ce/Mg/Al/O mixed oxide catalyst which displays high activity for simultaneous removal of NO and CO in the presence of O₂, H₂O and SO₂ under the conditions similar to those found in the dense phase bed of FCC.

2. Experimental

Cu/Ce/Mg/Al/O was prepared by co-precipitation of an aqueous solution of Cu(NO₃)₂·6H₂O, Ce(NO₃)₃·6H₂O, Mg(NO₃)₂·6H₂O and Al(NO₃)₃·9H₂O (total cation concentration of 1 M) with an aqueous solution of NaOH and Na₂CO₃ (CO₃²⁻-to-Al molar ratio of 0.5). The detailed procedure is described elsewhere [14–17]. The precipitate was filtered, washed with water and dried at 120 °C for 12 h, and then calcined in air at 750 °C for 3 h. The resulting product was designated as CuCe-cat. Cu-cat or Ce-cat catalyst was prepared using the same procedure except Ce(NO₃)₃·6H₂O or Cu(NO₃)₂·6H₂O, respectively, which was not included.

The catalytic reaction tests were carried out in a fixed bed quartz reactor with a porous frit in flow conditions. The quartz reactor was loaded with 150 mg (particulate size: 0.45–0.90 mm) of catalyst. The composition of the feed gas was regulated by mass flow controllers (Brooks 5058). A typical feed contained 600 ppm NO, 1.4 vol.% CO and 0.5% O₂ (similar to the conditions in the dense phase bed of the FCC regenerator) with ultra-high purity He as diluent. When desired, 1% H₂O was added to the feed using a H₂O saturator. The effect of SO₂ was examined by introducing 500 ppm SO₂ into the reaction system. The total flow rate was 400 ml/min. The experiments were carried out under atmospheric pressure. A cold trap connected at the outlet of the reactor was used to remove

the water from the effluent gas. The composition of the feed or effluent gas was analyzed on-line with QGS-08B infrared analyzers (for NO) and a GC-8APT gas chromatograph with two columns (GDX303 for SO₂ and CO₂; 13X for CO, O₂, N₂) and a TCD detector. NO and CO conversions were calculated from the formation of N₂ and CO₂, respectively. The products were also monitored on-line by mass spectrometry (Balzers Oministar, Quadrupole) in some runs.

3. Results and discussion

The catalysts used in this work are listed in Table 1.

Fig. 1 shows the NO conversions as a function of temperature over Cu-cat and CuCe-cat in the absence and presence of O₂. It can be seen that for the NO+CO system, in the low temperature region (lower than 340 °C), CuCe-cat has a higher NO reduction activity (reaching 100% conversion at 315 °C) than Cu-cat, and the difference increases with temperature within that region. At high temperatures, NO conversions over both catalysts reach 100%. The addition of O₂ to the feed produces a completely different effect on the NO conversion over Cu-cat and CuCe-cat. The presence of O₂ enhances the activity of CuCe-cat while it decreases the activity of Cu-cat. The activity of Ce-cat for NO conversion (not shown in Fig. 1) is much lower than that of CuCe-cat or Cu-cat under the same conditions. The presence of O₂ reduces the activity of Ce-cat.

In order to clarify the effect of O₂ on the reaction of NO + CO over these catalysts, the co-adsorption of NO and CO and the influence of O₂ on the adsorption of NO and CO were investigated by IR spectroscopy. Fig. 2 shows the IR spectra of NO and CO co-adsorption on CuCe-cat at room temperature. There is an intense band at 2118 cm⁻¹ with several

Table 1
The physico-chemical properties of samples^a

Catalyst	Composition (wt.%)				S _{BET} (m ² g ⁻¹)	Pore volume (ml g ⁻¹)
	MgO	Al ₂ O ₃	CuO	CeO ₂		
Cu-cat	62.0	29.3	8.4		184	0.68
Ce-cat	60.0	29.0		9.1	160	0.59
CuCe-cat	56.0	26.0	7.2	8.7	169	0.93

^a Mg to Al atomic ratio is about 2.7 for all samples.

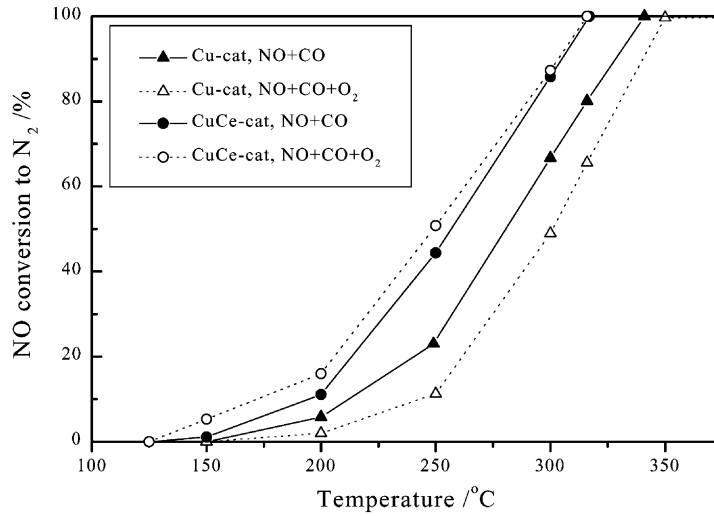


Fig. 1. NO conversions as a function of temperature over Cu-cat and CuCe-cat catalysts in the absence and presence of O₂. Reaction conditions: 600 ppm NO, 1.4% CO, 0.5% O₂; total flow rate: 400 ml/min.

weak bands at 1888, 1875, and 2355 cm⁻¹, respectively (Fig. 2A). The band at 2118 cm⁻¹ is ascribed to CO ligated to Cu⁺ sites [18] and the band at 1888 cm⁻¹ corresponds to the adsorption of NO on Cu²⁺ [19]. The 1875 cm⁻¹ band is attributed to

gaseous NO and the 2355 cm⁻¹ band is tentatively attributed to the adsorption of N₂O [20]. After subsequent evacuation up to 10⁻² Pa at room temperature, the 2118 cm⁻¹ band decreases and shifts to a lower frequency of 2102 cm⁻¹ while the bands at 1888 and

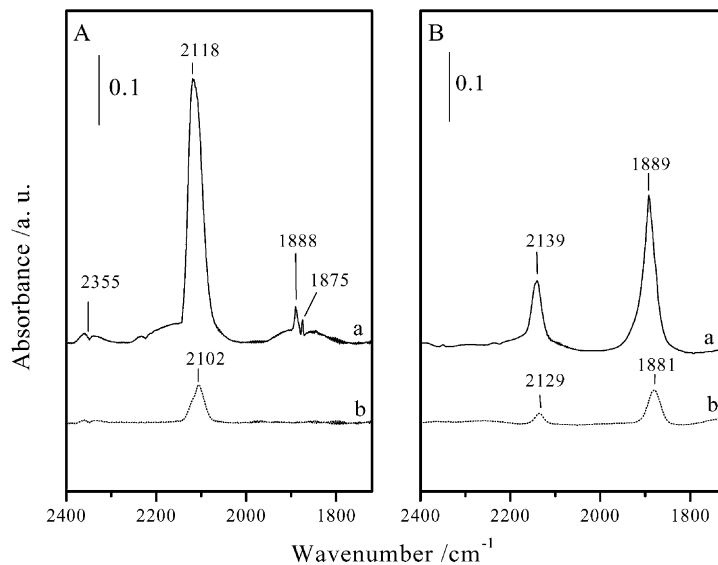


Fig. 2. IR spectra of NO and CO co-adsorption on CuCe-cat at room temperature. A: $P_{\text{NO}+\text{CO}} = 4.0 \text{ kPa}$, $P_{\text{NO}}:P_{\text{CO}} = 1:2$; B: $P_{\text{NO}+\text{CO}+\text{O}_2} = 4 \text{ kPa}$, $P_{\text{NO}}:P_{\text{CO}}:P_{\text{O}_2} = 1:3:1$ (a): after 25 min adsorption at the conditions of A or B; (b): followed by evacuation to 10⁻² Pa.

Table 2
Influences of the addition of water vapor and SO₂ on the NO conversions over the three catalysts

Catalyst	NO conversion (%) ^a								
	250 °C		300 °C		550 °C		720 °C		
	1	2	1	2	1	2	1	2	3
Cu-cat	11.3	0	49.0	1.6	97.8	98.5	98.7	100	31.4
Ce-cat	0	0	0	0	51.6	52.1	100	100	16.2
CuCe-cat	50.8	100	86.9	100	100	100	100	100	100

^a 1: NO + CO + O₂; 2: NO + CO + O₂ + H₂O; 3: NO + CO + O₂ + H₂O + SO₂. 1 and 2: after the reactions reach steady state; 3: after 40 min reaction.

1875 cm⁻¹ disappear completely. The shift of the 2118 cm⁻¹ band upon evacuation is attributed to the decrease of surface coverage of CO. Fig. 2B shows the effect of O₂ on the NO and CO adsorption. After introducing O₂ into the system, the band corresponding to the CO adsorption on Cu⁺ decreases significantly in intensity (by a factor of 4). However, it is interesting to note that the band assigned to NO adsorption on Cu²⁺ increases by a factor larger than 5. This indicates that the addition of a small amount of O₂ enhances the adsorption of NO. After evacuation, both bands shift to a slightly lower frequency while they decrease in intensity. As reported in our previous paper [14], a large number of Cu⁺ ions—active for CO adsorption—are formed during the calcination of CuCe-cat as a result of the strong synergistic effect between copper and cerium ions. The presence of O₂ oxidizes some Cu⁺ ions into Cu²⁺ ions, which are not active for CO adsorption but are active for NO adsorption [19]. This explains the corresponding decreased intensity of the band at 2118 cm⁻¹ and the increased intensity of the band at 1888 cm⁻¹. Over Cu-cat, most of the copper ions are present as Cu²⁺ ions [14]. Over Ce-cat, no NO and CO adsorption are detected

by IR spectroscopy (not shown here). The exact ν_{CO} band position is considered to be dependent on the environment of the Cu⁺ ion to which CO is bound. The shift from 2118 to 2139 cm⁻¹ with the addition of O₂ is due to a greater concentration of Cu²⁺ ions in positions surrounding the Cu⁺ adsorption site [21].

The influences of the addition of water vapor and SO₂ on the NO conversions over these three catalysts were examined and the results are presented in Table 2. When 1% H₂O is introduced into the feed, Cu-cat loses its activity completely at 250 °C; the activity at 300 °C also drops drastically. However, at the same conditions (250 or 300 °C), it is interesting to note that the addition of H₂O enhances the activity of CuCe-cat significantly. At high temperatures, the presence of H₂O has no significant effect on the NO conversion. At 720 °C, the addition of SO₂ results in a drastic decline of NO conversion, from 100 to 31.4% for Cu-cat and from 100 to 16.2% for Ce-cat during the first 40 min. These data indicate that both catalysts are rapidly poisoned by SO₂. However, the presence of SO₂ in the feed has no adverse effect on the NO conversion over CuCe-cat which maintains 100% conversion. Even after a 24 h run, no decline in conversion is observed.

Table 3
CO conversions under different reaction conditions

Catalyst	CO conversion (%) ^a								
	250 °C		550 °C		720 °C				
	1	2	1	2	1	2	3		
Cu-cat	60.9	30.8	75.7	93.7	75.7	95.3	74.4		
Ce-cat	12.0	0	73.6	76.2	75.6	86.8	46.1		
CuCe-cat	73.5	85.6	75.7	95.1	75.7	95.8	96.1		

^a 1: CO + O₂ + NO; 2: CO + O₂ + H₂O + NO; 3: CO + O₂ + H₂O + NO + SO₂. 1 and 2: after the reactions reach steady state; 3: after 40 min reaction.

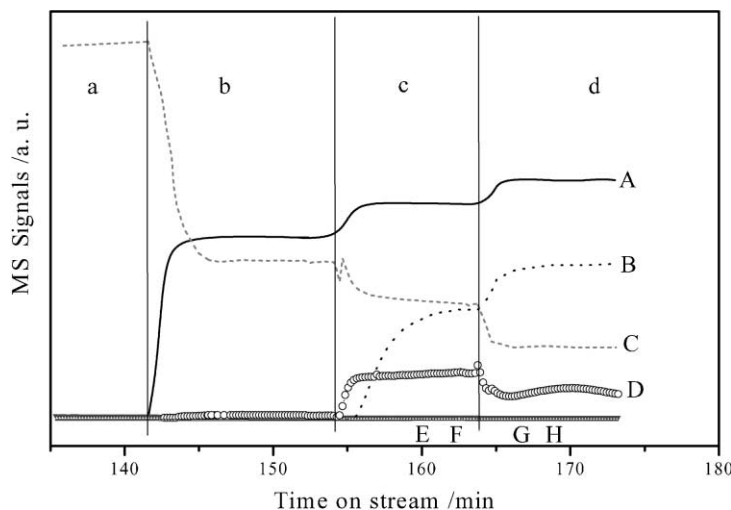


Fig. 3. Effects of the addition in sequence of O_2 , H_2O and SO_2 on NO and CO conversions over CuCe-cat at $720^\circ C$. (a): NO (600 ppm)+CO (1.4%) system; (b): introducing 0.5% O_2 into (a) system; (c): introducing 1% H_2O into (b) system; (d): introducing 500 ppm SO_2 into (c) system. A: CO_2 ; B: H_2O ; C: CO; D: H_2 ; E: O_2 ; F: NO; G: H_2S ; H: COS.

Table 3 gives CO conversions under different reaction conditions. At $250^\circ C$, CuCe-cat and Cu-cat have much higher CO oxidation activity than Ce-cat. The presence of H_2O increases CO conversion over CuCe-cat while drastically reducing it over Cu-cat or Ce-cat. At $720^\circ C$, the addition of H_2O promotes CO conversion over all the three catalysts. The presence of SO_2 in the NO+CO+ O_2 + H_2O system has no effect on the reaction between CO and O_2 over Cu-cat, but deactivates this catalyst completely for the reaction of CO+ H_2O (this is also confirmed by MS data; not shown here). For Ce-cat, both the reactions of CO+ O_2 and CO+ H_2O are suppressed significantly. However, the CO conversion over CuCe-cat increases slightly with the addition of SO_2 . The effects of O_2 , H_2O and SO_2 on the CO and NO conversions over CuCe-cat can be seen in detail in Fig. 3. When 0.5% O_2 is introduced into the system, it is consumed completely by CO, concomitant with the formation of CO_2 . With the addition of water vapor, the signal of CO decreases and that of CO_2 increases. Meanwhile, H_2 is detected. The addition of SO_2 has no effect on the reaction of CO+ O_2 , but slightly inhibits the reaction of CO+ H_2O . The increase of the CO_2 signal is derived from the reaction of $CO + SO_2 \rightarrow CO_2 + S$, as evidenced by the condensate of sulfur in the

reactor outlet. No undesirable COS and H_2S are detected in the whole experiment.

4. Remarks

From the preceding results, it can be seen that CuCe-cat shows higher catalytic activity and stability than Cu-cat and Ce-cat for the simultaneous removal of NO and CO in the presence of O_2 , H_2O and SO_2 . The addition of O_2 increases NO conversion over CuCe-cat because it oxidizes some Cu^+ ions to Cu^{2+} ions which are active for NO adsorption. The different influence of H_2O on NO and CO conversion derives from the different activities of the catalysts for the water-gas shift reaction (WGS, $CO + H_2O \rightarrow CO_2 + H_2$). With many more Cu^+ sites for CO adsorption, CuCe-cat exhibits a high WGS activity at low temperature while Cu-cat and Ce-cat require high temperature [22]. At low temperature, the strong adsorption of H_2O on Cu^{2+} or Cu^+ sites will inhibit the adsorption of NO or CO over Cu-cat; however, for CuCe-cat, WGS leads to the increase of CO conversion and the formation of H_2 which is active for NO reduction at low temperature. The presence of SO_2 increases the CO conversion and has no adverse effect

on NO conversion over CuCe-cat at 720 °C; however, it significantly decreases both NO and CO conversions over Cu-cat and Ce-cat. All of these promoted performances of CuCe-cat result from the strong interaction of copper and cerium which gives rise to a large number of Cu⁺ ions [14]. SO₂ cannot block CO adsorption on Cu⁺ ions [23]. Further work is underway to elucidate the reaction mechanism in detail.

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